

**Table 2-18W**  
**ALLOWABLE STRESSES  $F/\Omega$  (k/in<sup>2</sup>) FOR BUILDING-TYPE STRUCTURES (WELDED)**

<u>Axial Tension</u>	Section	$F/\Omega$
axial tension stress on net effective area	D.2b	12.3
axial tension stress on gross area	D.2a	6.7
<u>Shear or torsion</u>		
Shear or torsion rupture	G, H.2	7.4
<u>Bearing</u>		
bolts or rivets on holes	J.3.6a, J.4.6	24.6
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	16.4
screws in holes	J.5.5.1	16.0

6061 - T6      ASTM B209 0.010 to 4.000 in. thick  
 6061 - T651    ASTM B209 0.010 to 4.000 in. thick  
 6061 - T6      ASTM B210 0.025 to 0.500 in. thick  
 6061 - T6      ASTM B211 0.125 to 8.000 in. thick  
 6061 - T651    ASTM B211 0.125 to 8.000 in. thick  
 6061 - T6      ASTM B632 0.010 to 0.625 in. thick  
 6061 - T6      ASTM B221, B241, B429  
 6061 - T6510    ASTM B221  
 6061 - T6511    ASTM B221  
 6061 - T6      ASTM B247 0.000 to 4.000 thick  
 6061 - T6      ASTM B308 0.062 thick and greater  
 6351 - T5      ASTM B221 0.000 to 1.000 in. thick

$$F_{tyw} = 11 \text{ k/in}^2 \quad E = 10,100 \text{ k/in}^2$$

$$F_{cyw} = 11 \text{ k/in}^2 \quad k_t = 1$$

$$F_{tuw} = 24 \text{ k/in}^2$$

For thicknesses > 0.375" welded with 4043, 5554,  
or 5654 alloy filler

	$\lambda$	$F/\Omega$ for $\lambda \leq \lambda_1$	$\lambda_1$	$F/\Omega$ for $\lambda_1 < \lambda < \lambda_2$	$\lambda_2$	$F/\Omega$ for $\lambda \geq \lambda_2$	
<u>Axial Compression - member buckling</u>	E.2	$kL/r$	6.7	22.3	$0.00003 \lambda^2 - 0.040 \lambda + 7.5$	157	$51,352/\lambda^2$
<u>Flexure - lateral-torsional buckling</u>	F.4	see F.4.2	-	see F.4	157	$60,414/\lambda^2$	
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	$b/t$	6.7	9.8	$8.6 - 0.198 \lambda$	29	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	$b/t$	6.7	9.8	$8.6 - 0.198 \lambda$	21.8	$94/\lambda$
flat elements supported on both edges	B.5.4.2	$b/t$	6.7	30.8	$8.6 - 0.063 \lambda$	68	$293/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	$\lambda_s$	6.7	22.3	$7.4 - 0.031 \lambda$	157	$60,414/\lambda^2$
round hollow elements	B.5.4.5	$R_p/t$	6.7	52.2	$8.5 - 0.257 \lambda^{1/2}$	389	$3,776/(\lambda k_r)^\dagger$
flat elements - direct strength method	B.5.4.6	$\lambda_{eq}$	6.7	49.2	$8.6 - 0.040 \lambda$	109	$468/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	$b/t$	10.0	36.3	$11.4 - 0.039 \lambda$	145	$830/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	$b/t$	10.0	6.7	$11.4 - 0.212 \lambda$	36	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	$b/t$	10.0	81.4	$11.4 - 0.018 \lambda$	326	$1,861/\lambda$
pipes and round tubes	B.5.5.4	$R_p/t$	$12.8 - 0.606 \lambda^{1/2}$	149.9	$8.5 - 0.257 \lambda^{1/2}$	389	$3,776/(\lambda k_r)^\dagger$
flat elements - direct strength method	B.5.5.5	$\lambda_{eq}$	$M_{np}/S_{xc}$	49.2	see B.5.5.5	145	$468/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	$b/t$	4.0	51.9	$5.2 - 0.023 \lambda$	149	$38,665/\lambda^2$
flat elements supported on one edge	G.3	$b/t$	4.0	21.6	$5.2 - 0.056 \lambda$	62	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	$\lambda_p^*$	4.0	91.3	$6.8 - 0.030 \lambda$	149	$50,264/\lambda^2$
<u>Torsion - pipes and round or oval tubes</u>	H.2.1	$\lambda_p^*$	4.0	51.9	$5.2 - 0.023 \lambda$	149	$38,665/\lambda^2$

\* $\lambda_p = 2.9(R_p/t)^{5/8}(L/R_b)^{1/4}$   
 $\dagger k_r = (1 + \lambda^{1/2}/35)^2$

**Table 2-19W**  
**ALLOWABLE STRESSES  $F/\Omega$  (k/in<sup>2</sup>) FOR BUILDING-TYPE STRUCTURES (WELDED)**

<u>Axial Tension</u>	Section	$F/\Omega$
axial tension stress on net effective area	D.2b	12.3
axial tension stress on gross area	D.2a	9.1
<u>Shear or torsion</u>		
Shear or torsion rupture	G, H.2	7.4
<u>Bearing</u>		
bolts or rivets on holes	J.3.6a, J.4.6	24.6
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	16.4
screws in holes	J.5.5.1	16.0

**6061 - T6**      **ASTM B209 0.010 to 4.000 in. thick**  
**6061 - T651**    **ASTM B209 0.010 to 4.000 in. thick**  
**6061 - T6**      **ASTM B210 0.025 to 0.500 in. thick**  
**6061 - T6**      **ASTM B211 0.125 to 8.000 in. thick**  
**6061 - T651**    **ASTM B211 0.125 to 8.000 in. thick**  
**6061 - T6**      **ASTM B632 0.010 to 0.625 in. thick**  
**6061 - T6**      **ASTM B221, B241, B429**  
**6061 - T6510**    **ASTM B221**  
**6061 - T6511**    **ASTM B221**  
**6061 - T6**      **ASTM B247 0.000 to 4.000 thick**  
**6061 - T6**      **ASTM B308 0.062 thick and greater**  
**6351 - T5**      **ASTM B221 0.000 to 1.000 in. thick**

$$F_{tyw} = 15 \text{ k/in}^2 \quad E = 10,100 \text{ k/in}^2$$

$$F_{cyw} = 15 \text{ k/in}^2 \quad k_t = 1$$

$$F_{tuw} = 24 \text{ k/in}^2$$

For thicknesses  $\leq 0.375$ " welded with 4043, 5554, or 5654 and for any thickness welded with 5183, 5356, or 5556

		$\lambda$	$F/\Omega$ for $\lambda \leq \lambda_1$	$\lambda_1$	$F/\Omega$ for $\lambda_1 < \lambda < \lambda_2$	$\lambda_2$	$F/\Omega$ for $\lambda \geq \lambda_2$
<u>Axial Compression - member buckling</u>	E.2	$kL/r$	9.1	21.8	$0.00007 \lambda^2 - 0.066\lambda + 10.5$	133	$51,352/\lambda^2$
<u>Flexure - lateral-torsional buckling</u>	F.4	see F.4.2		-	see F.4	133	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	$b/t$	9.1	9.0	$12.0 - 0.327\lambda$	25	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	$b/t$	9.1	9.0	$12.0 - 0.327\lambda$	18.4	$111/\lambda$
flat elements supported on both edges	B.5.4.2	$b/t$	9.1	28.2	$12.0 - 0.105\lambda$	58	$346/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	$\lambda_s$	9.1	21.8	$10.2 - 0.051\lambda$	133	$60,414/\lambda^2$
round hollow elements	B.5.4.5	$R_p/t$	9.1	46.4	$11.8 - 0.396\lambda^{1/2}$	389	$3,776/(\lambda k_r)^\dagger$
flat elements - direct strength method	B.5.4.6	$\lambda_{eq}$	9.1	45.1	$12.0 - 0.065\lambda$	92	$554/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	$b/t$	13.6	36.2	$16.0 - 0.065\lambda$	123	$982/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	$b/t$	13.6	6.7	$16.0 - 0.350\lambda$	30	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	$b/t$	13.6	81.2	$16.0 - 0.029\lambda$	275	$2,201/\lambda$
pipes and round tubes	B.5.5.4	$R_p/t$	$17.7 - 0.933\lambda^{1/2}$	120.8	$11.8 - 0.396\lambda^{1/2}$	389	$3,776/(\lambda k_r)^\dagger$
flat elements - direct strength method	B.5.5.5	$\lambda_{eq}$	$M_{np}/S_{xc}$	45.1	see B.5.5.5	123	$554/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	$b/t$	5.5	47.5	$7.3 - 0.038\lambda$	126	$38,665/\lambda^2$
flat elements supported on one edge	G.3	$b/t$	5.5	19.8	$7.3 - 0.092\lambda$	53	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	$\lambda_p^*$	5.5	80.0	$9.5 - 0.050\lambda$	126	$50,264/\lambda^2$
<u>Torsion - pipes and round or oval tubes</u>	H.2.1	$\lambda_p^*$	5.5	47.5	$7.3 - 0.038\lambda$	126	$38,665/\lambda^2$

$$*\lambda_p = 2.9(R_p/t)^{5/8} (L/R_b)^{1/4}$$

$$\dagger k_r = (1 + \lambda^{1/2}/35)^2$$